

## Requirements and application of UHF PD monitoring systems for gas insulated systems





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## **Chapter 1 – Introduction**

## Scope of the activity

CIGRE WG D1.66 was tasked with defining requirements for GIS Partial Discharge Monitoring systems to ensure that signals from incipient PD defects are reliably detected, monitored, and interpreted, so that asset managers can take prompt and appropriate actions to prevent equipment malfunction

UHF PDM systems are in widespread use throughout the world. In the last 10 years more than 700 systems have been installed on more than 85,000 UHF sensors (representative samples)



For one GIS owner, the appropriate strategy may be to install PDM systems on all of their GIS installations at or above a specified voltage level for the whole of the actual operational lifetime, while for another GIS owner, it may be optimal to install PDM systems based on the risk and criticality of individual substations

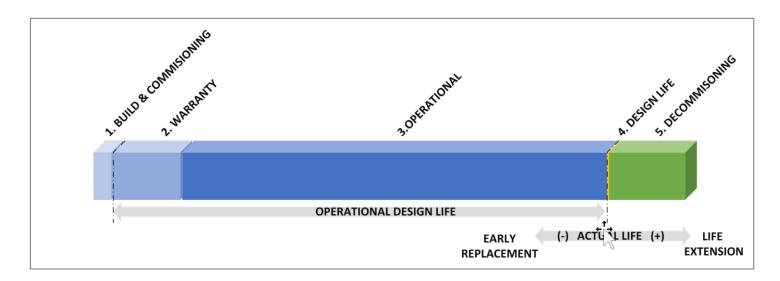


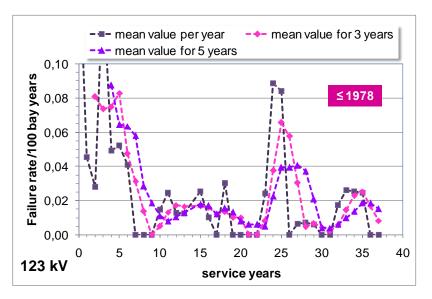


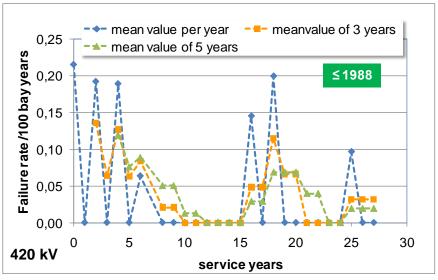
Figure 1 - The five value stages of GIS ownership

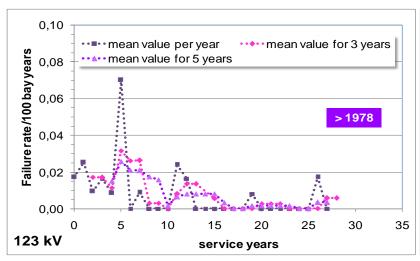
		manufacturing period	<1979	1979- 1983	1984- 1988	1989- 1993	1994- 1998	1999- 2003	2004- 2007		
CIGRE , 3 <sup>rd</sup> inquiry 3		MaF, per 100 bay years	2.0	1.25	0.65	0.125	0.15	0.1	0.3		
	100 - 200 kV	thereof dielectric failures 1)	29%	20%	50%	50%	60%	43%	86%		
	200 111	dielectric failures per 100 bay years 1)	0,58	0,25	0,33	0,06	0,09	0,04	0,26		
	300 - 500 kV	MaF, per 100 bay years	4.0	2.0	1.3	0.6	0.4	0.3	0.55		
		thereof dielectric failures 1)	23%	23%	11%	45%	70%	82%	40%		
		dielectric failures per 100 bay years 1)	0,92	0,46	0,14	0,27	0,28	0,25	0,22		
GIS	GIS 123 kV	dielectric failures, per 100 bay years	0.2	0.04		0.05		0.0			
Userforum	420 kV	dielectric failures, per 100 bay years	0.0	0.11		0.09					
updated based on detailed data of the 3rd CIGRE inquiry											

Figure 2 - Comparison of the reliability data presented in the 3rd CIGRE international enquiry [and collected by the GIS Userforum









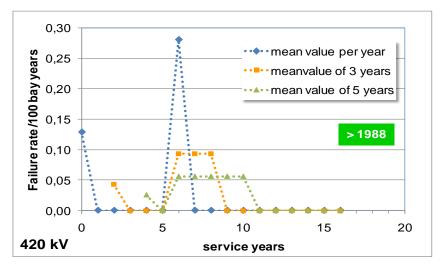
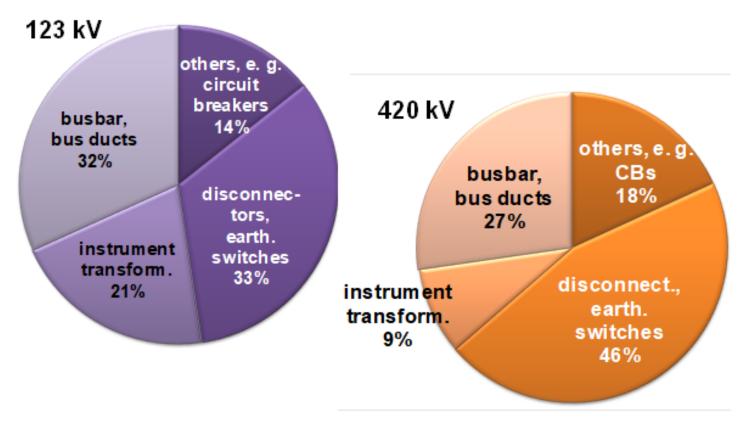




Figure 3 – Failure rates in GIS



In modern GIS, the failure rate should decrease, owing to lessons learned, improvements in design, and quality of the components installed

Inversely, if the GIS is PD-free, then the probability of failure is lower; PDM use contributes more to asset management decision making for maintenance and end-of-life prediction.

Figure 4 - Main root causes of failures in 123 kV and 420 kV GIS



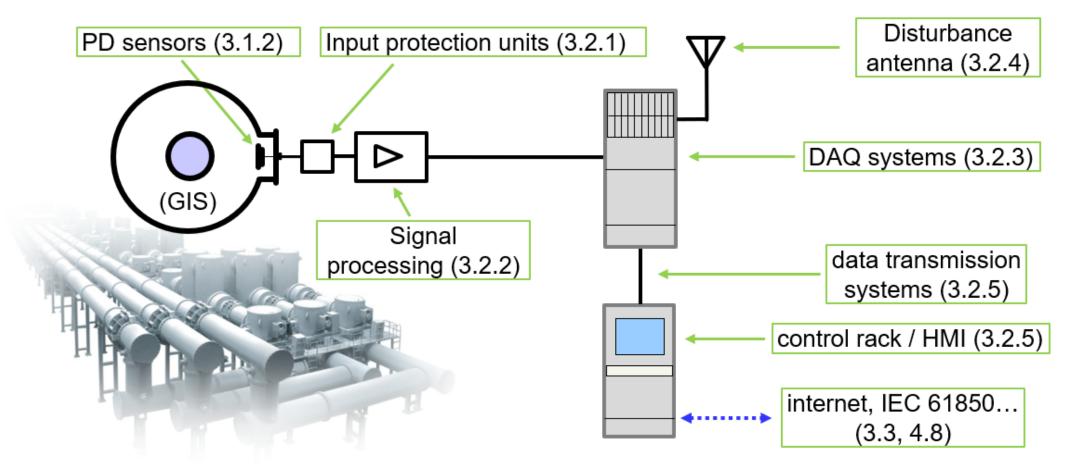


Figure 5 - General Architecture of current PD monitoring systems









Figure 6 - Examples of GIS/GIL UHF PD sensors

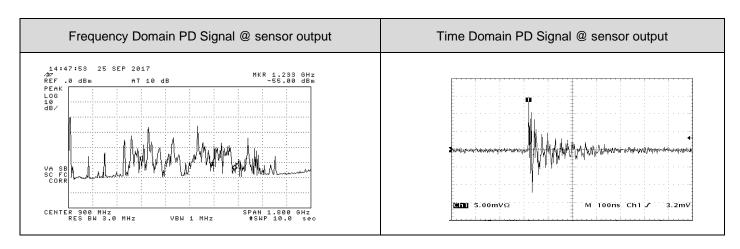
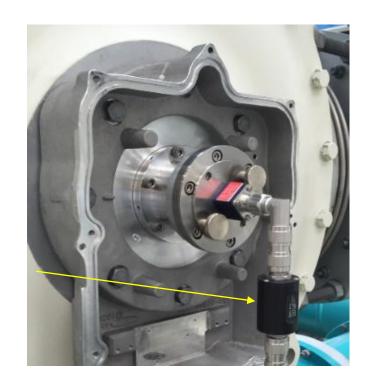




Figure 7 - UHF impulse measured at the output of an internal sensor



Input protection module



Acquisition system



Indoor system with 120 channels





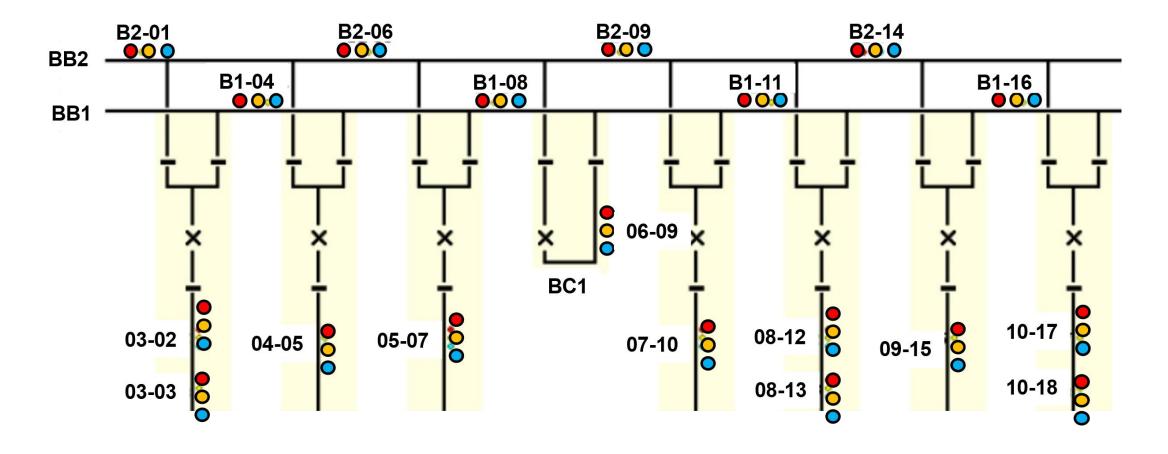


Figure 13 - Example of 400 kV GIS PD monitoring system overview screen



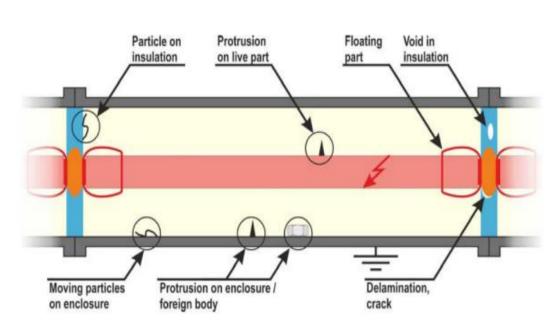


Figure 8 – Typical defects in GIS installation

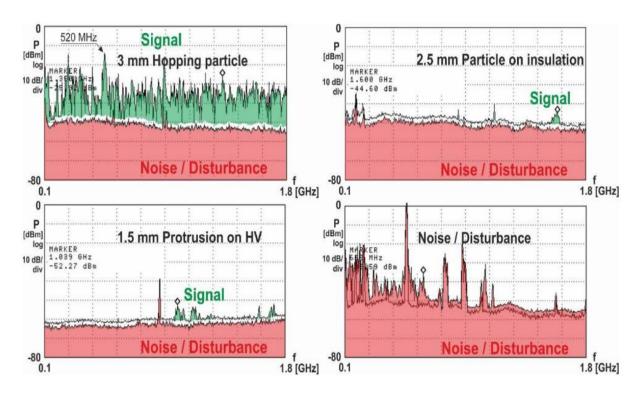


Figure 9 - Examples of UHF spectra for different defects



Figure 14 - Examples of phase-resolved PD data patterns



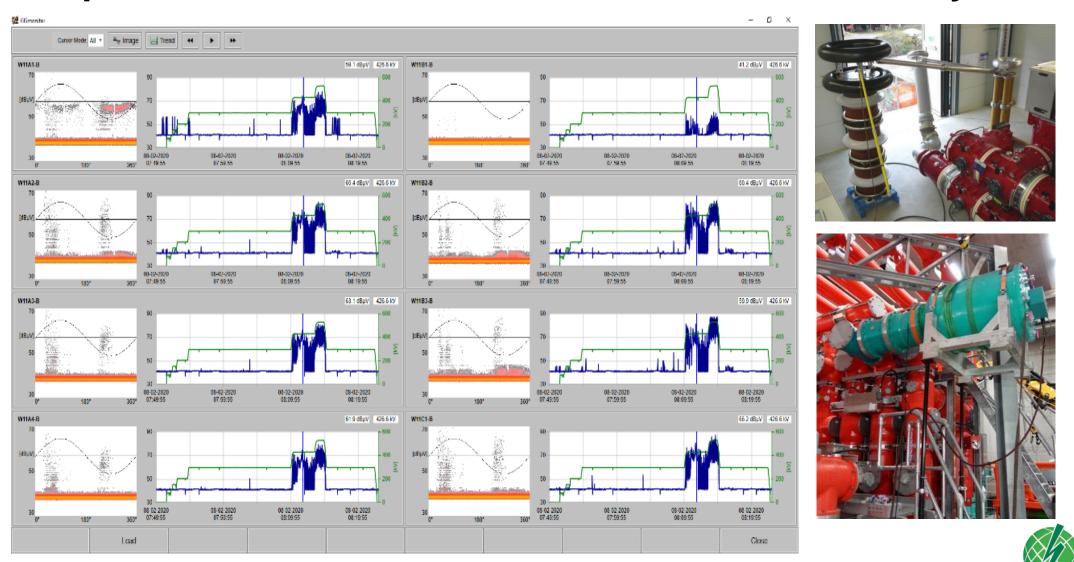


Figure 15 - Screenshot from a PDM system recording data during HV commissioning test

For power system expertise

#### Functions and features of the most advanced PDM systems

Applicable for all kinds of UHF sensors; internal sensors are preferable owing to better signal-to-noise capability

With multi-channel synchronous PDM Systems, all PD pulses/events are independently acquired.

Capable of performing CIGRE TB 654 UHF Sensitivity Procedure Steps 1 and 2

Provide external communication interfaces in accordance with the appropriate applicable standards (e.g. IEC 61850)

Integrate PDM systems on GIS of different voltage levels into one general overview control system

Support the on-site HV acceptance test during commissioning of the GIS; normally a separate, purposely designed HV test mode incl. voltage/PD recording vs. time

PDMS GUI offers a user-friendly single line diagram; GIS Overview shows suspicious PD signal activity at a glance

Are scalable/extendable

Provide remote access to the PDM system

Most systems provide external UHF disturbances cancellation features (both software- and hardware-based)

Are safe in operation (protection front end modules) and pose no risk to insulation integrity of GIS/GIL

#### **Technical weaknesses:**

External noise discrimination is often challenging to setup; external disturbances often generate false alarms

Expert systems are not efficient or accurate

Alert/warning procedure do not consider results from the sensitivity check and from the signal profile measurements

#### Other types of weaknesses:

Present PDM systems run in stand-alone mode (i.e. they operate in isolation from other monitoring systems)

FAT for PDM systems are not defined or standardized, making it difficult to assign and assess pass/fail criteria

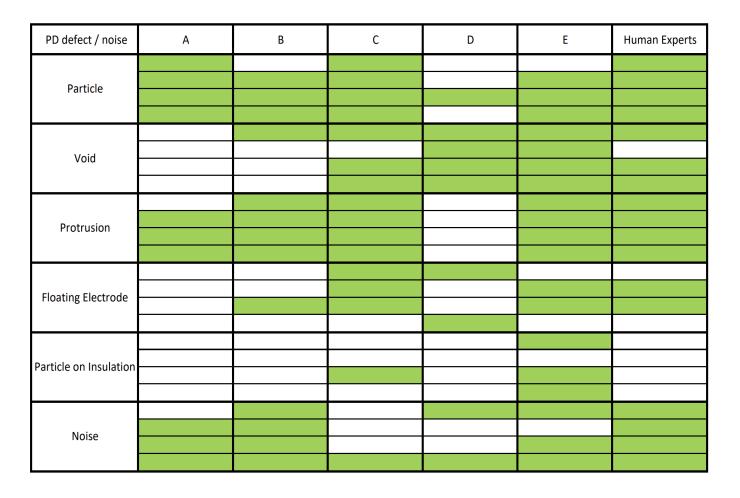
Data format and displayed information (graphs, trends, PD patterns, etc.) are not standardized and not compatible between systems of different vendors; PD amplitude reference points are not clearly specified;

Computers and some DAQ boards of PDM systems have to be replaced after several years of operation; long-time quality and robustness are limited, component obsolescence (a problem intrinsic to electronic hardware)

By definition, use of multiplexing detection methodologies raises the possibility of missing some intermittent PD signals Use of narrow-band detection methodology without spectrum analysis (wideband scanning) risks missing severely frequency bandlimited PD signals

Figure 15 – Weaknesses and Strengths of current PDM systems





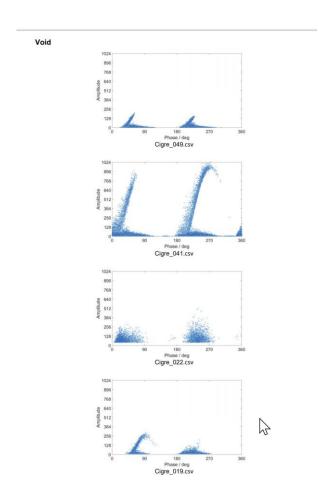
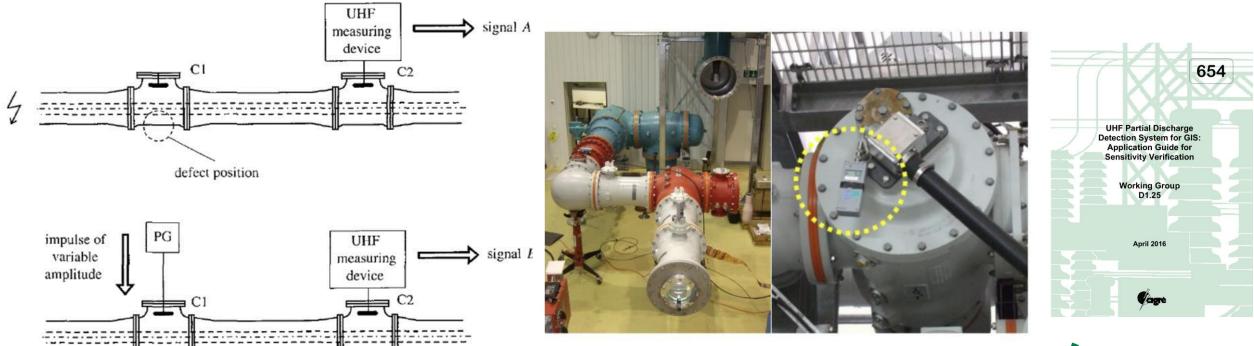


Figure 16 - Results of PD identification by pattern recognition algorithms (A-E) and human experts (green box indicates correct identification)



(based on the evaluation of defined PRPS data sets representing PD signals and noise)

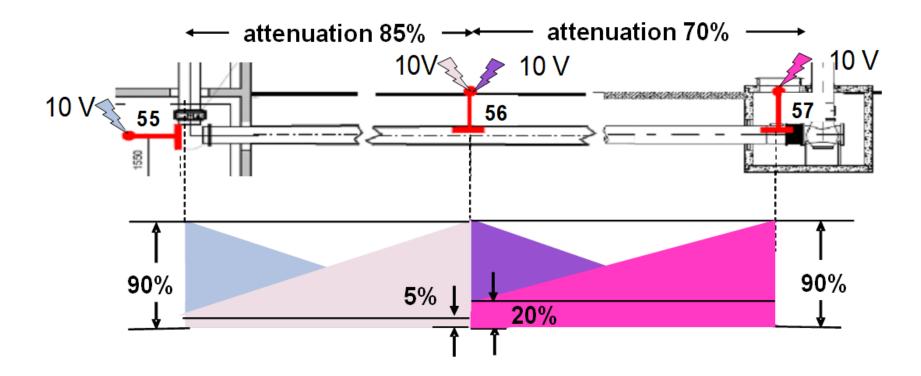
## **UHF PD measurements in GIS/GIL: System sensitivity check**



CISTE For power system expertise

Test set-up for UHF Sensitivity check according to CIGRE requirements (TB 654)

#### **PD Signal profile measurements**



The attenuation profiles are an approximation; they are determined during the Step 2 test by injecting a pulse signal in one sensor, acquiring it at the next adjacent sensor and recording the received signal amplitude.

Figure 17 - PDM system commissioning – attenuation signal profile measurments



#### Warning and alert procedure

The determination of an appropriate alert level can be derived from the information gathered during the CIGRE TB 654 Sensitivity Verification Steps 1 and 2.

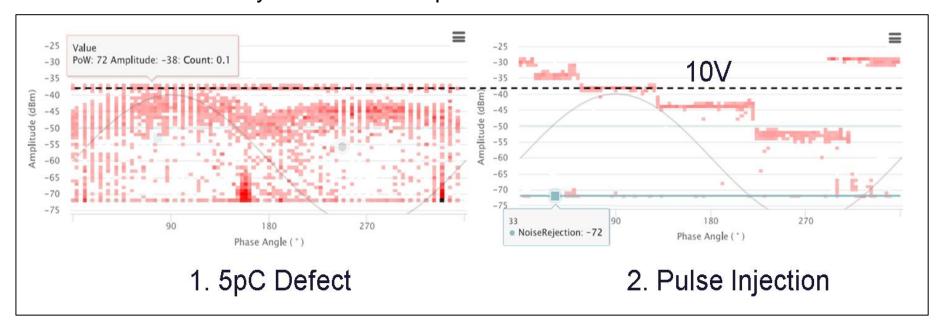
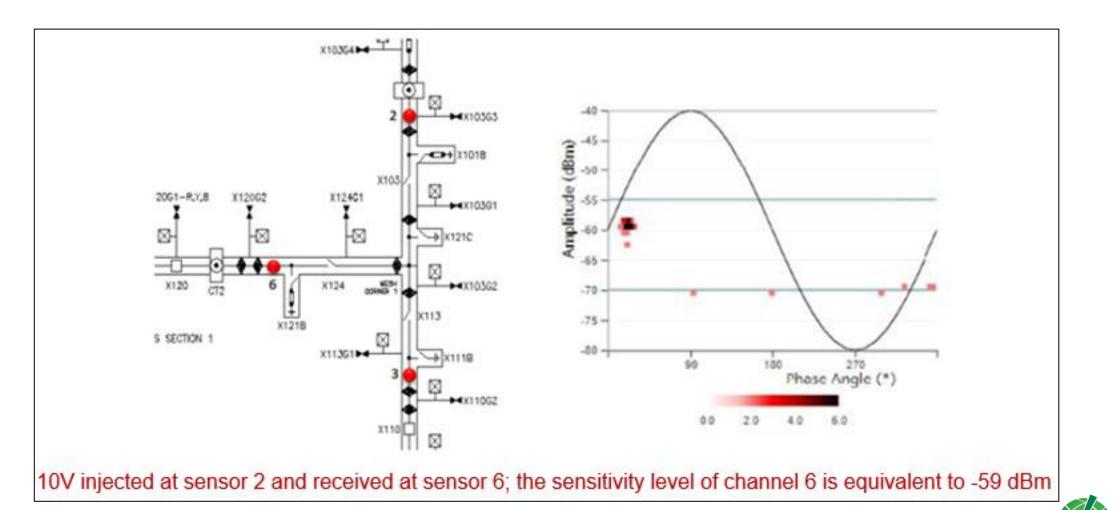


Figure 19 - Sensitivity Step 1 Test Result

A 5 pC mobile particle defect is measured with an amplitude of -37 dBm, corresponding to an artificial pulse magnitude of 10 V.





#### Warning and alert procedure

The data acquisition threshold, known as  $DT_B$ , can be set according to the results of the TB 654 Sensitivity Test Step 2. The threshold shall be between the sensitivity level  $A_s$ , and the background noise level. When there are multiple adjacent sensors, the lowest value of  $A_s$  shall be used.

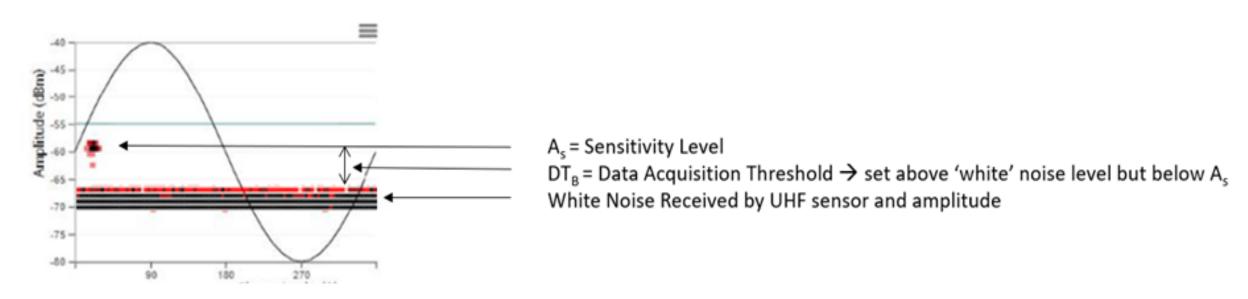


Figure 21 - Illustration of determination of DT<sub>B</sub>



#### Warning and alert procedure

If the values recorded by the PDM system during Step 1 are declared as *APD* and the attenuation between two sensors in Step 2 are measured and declared as *ATT*, then an alert level (*AL*) can be defined as follows:

$$AL = APD - \alpha ATT$$

The value of  $\alpha$  represents an estimation of the relative distance of the partial discharge source between two sensors. Typically, a value of  $\alpha = 0.5$  can be used to represent the attenuation of the signal at the mid-point of two sensors. If the same PD source can be detected at two adjacent sensors, it is possible to improve the estimate of  $\alpha$  and thus determine the alert level more accurately.



#### Warning and alert procedure

#### **Simplified Method**

Following the case study above, we can state that APD = -37 dBm and ATT = 22 dBm. Therefore, the alert threshold level for sensor 6 shall be:

$$AL = -37 - (0.5 \times 22) = -48 \ dBm$$

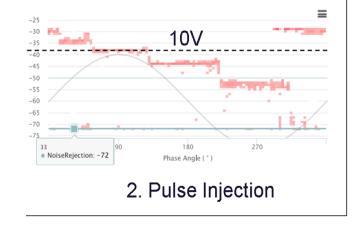
Only a partial discharge signal recorded at Sensor 6 of a value above -48 dBm can be declared as greater than or equal to 5 pC (assuming linear attenuation) and an alert may be raised. If the value is

less than -48 dBm, then the level shall be checked on Sensor 2, and an alert may still be raised. This

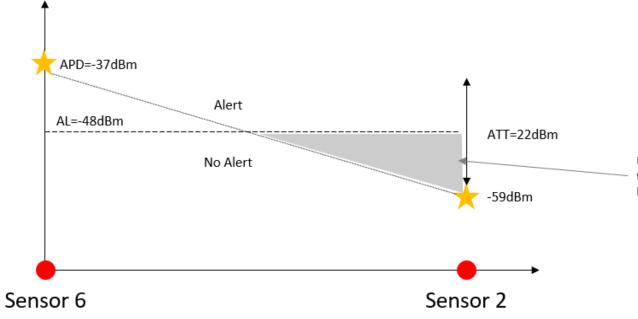
procedure is visualized in Figure 4.26.

For instances where a sensor has multiple adjacent sensors, then the lowest value for AL for each sensor pairing shall be used for that sensor, to ensure the 5 pC coverage at all points.

## Warning and alert procedure



Amplitude of received signal at Sensor 6 from 5pC discharge (dBm)



Discharge in Grey section is closer to Sensor 2, therefore alert shall be based upon that channel threshold





#### Warning and alert procedure

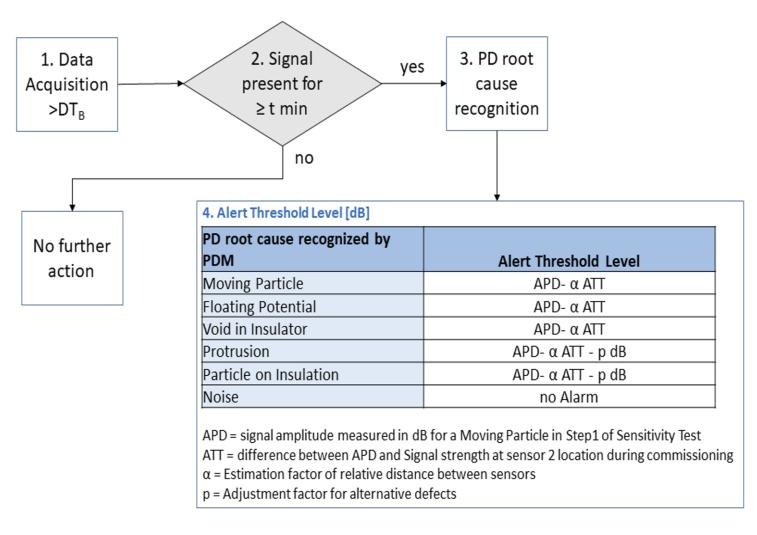
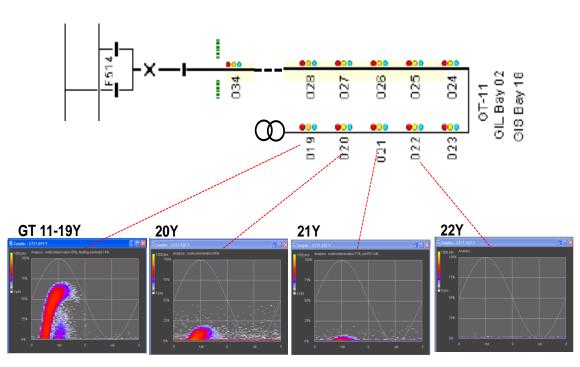




Figure 22 - Warning and alert procedure

#### **Risk assessment procedure**



The PD signal was acquired at service voltage and the PD inception not directly related to a transient voltage. The activity was continuous and its phase position stable.

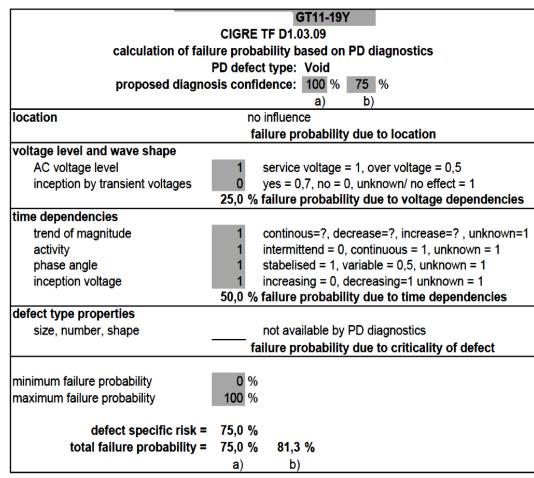
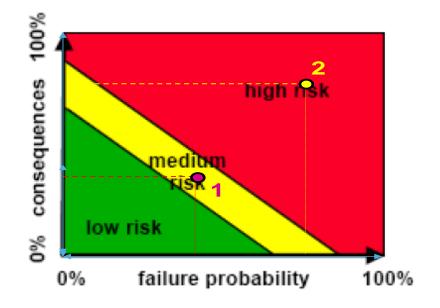


Figure 23 – Example of dielectric failure probability calculation according to TB 525



#### **Risk assessment procedure**

Example is related to a power station infeed, for which outage costs for non-delivered energy had been agreed, i.e. indicating the substation is of high importance. Moreover, spare parts were presumably not available and a long duration of repair work had to be assumed. Hence, high consequences of 80% were estimated.





## **Chapter 6 – Conclusions**

- New drivers and expectations for condition monitoring systems are described.
- The technical advantages and features of different monitoring solutions currently available on the market are shown and the minimum requirements for a GIS PDM system are given.
- One of the most pressing challenges facing GIS PDM systems is to significantly reduce the number of false alarms, and for this purpose, a novel warning/alert procedure is proposed. It recommends using the results from the CIGRE TB 654 UHF sensitivity check along with UHF signal attenuation profiles to set threshold values for each UHF sensor.
- Accurate and reliable automated PD defect type recognition plays a privotal role in both reducing false alarms and revealing defects which actually pose risk to operation and thus has to be further developed and implemented.

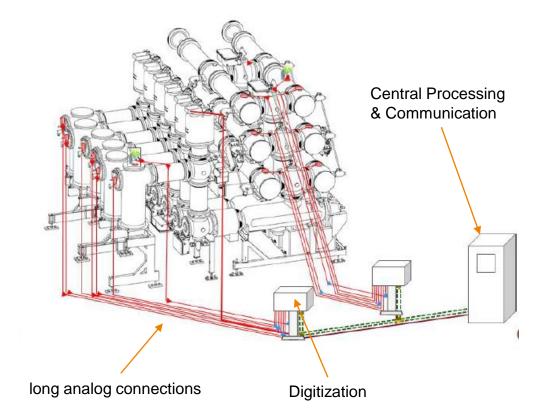


## **PARADIMO 100**

Ultra-high-frequency partial discharge monitoring system for GIS and GIL

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## Central Server Concept vs.



# **New IoT Concept**

short analog connections



Processing, Digitization & Communication in one unit close to the coupler

#### Your Benefits:

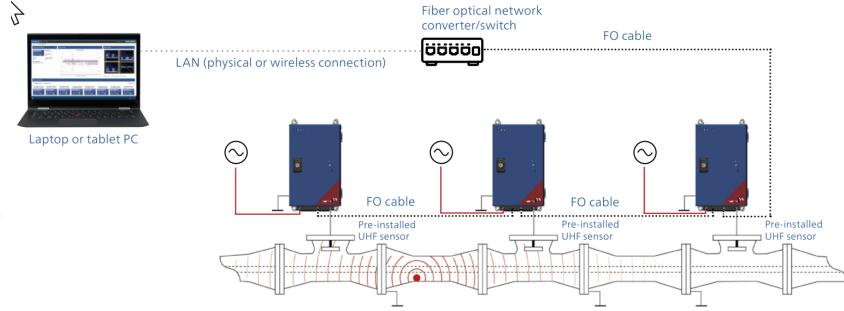
- Less HW required (e.g. no server)
- Less SW required (All-in-one Unit)
- High sensitivity due to short analog cables
- Easy integration into IT network



## **PARADIMO 100**

## **PD EXPERTISE** you can trust INSIDE Built-in processing, storage and communication Secure enclosure for Status LEDs indoor and outdoor use OMICRON 32 **UHF** sensor AC power Plug-and-play Ethernet (via connections: fiber optics)

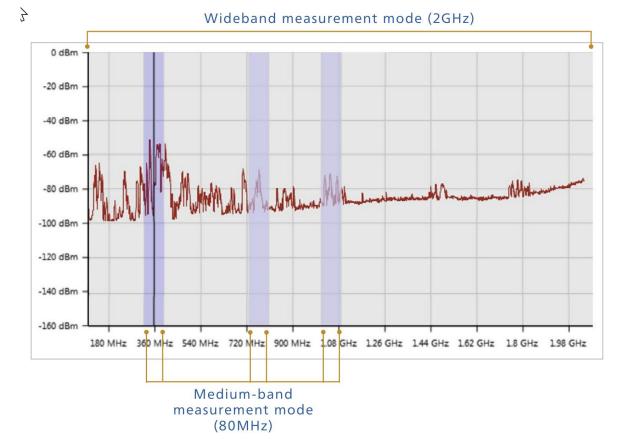
# Ultra-high-frequency PDM System for GIS and GIL



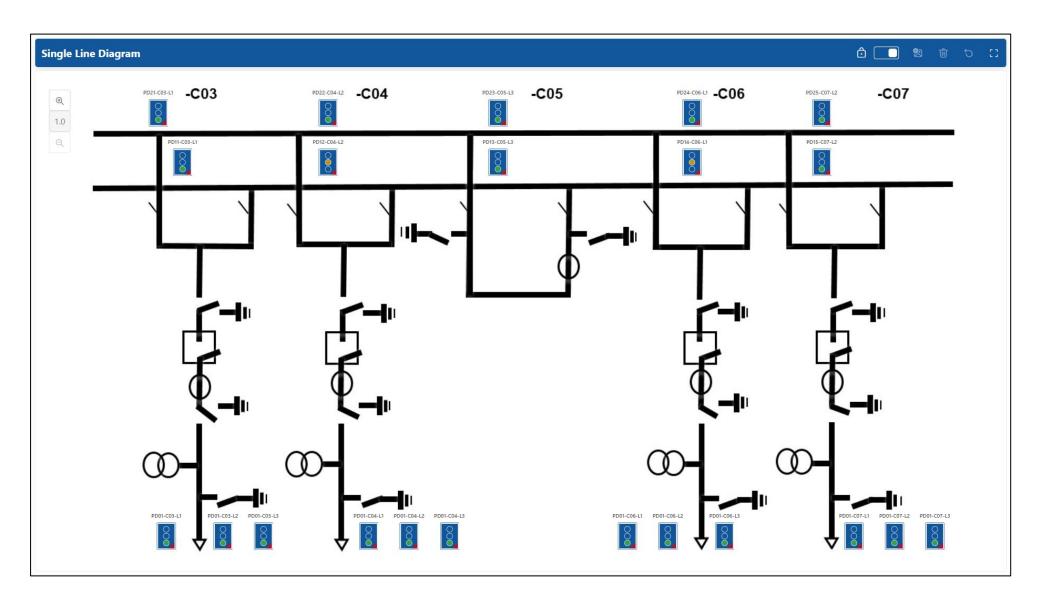
Connection of PARADIMO 100 devices via a fiber optical network converter/switch to a PC or tablet computer using a web browser for remote network access.

## **PARADIMO 100**



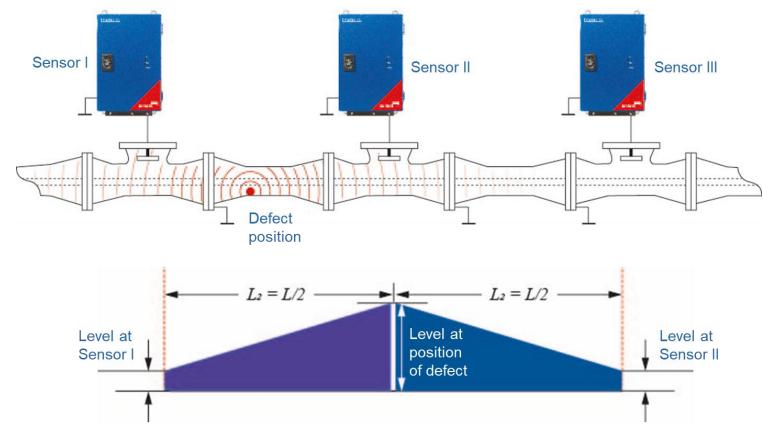


# **System Overview**



# **Smart alarming algorithm**

The alerting algorithm takes the attenuation between neighboring sensors into consideration for the continuous evaluation of monitored PD levels.



**Attenuation profile** – Linear approximation of the attenuation profile for a PD defect location in the middle of 2 sensors (Cigrè TB 654).

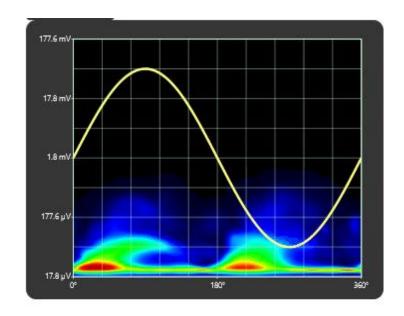
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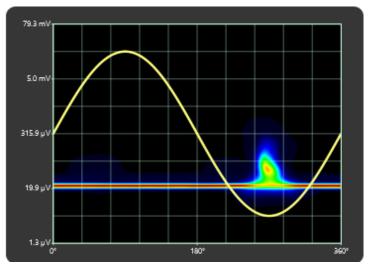
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## **UHF PDM system**









# Thank you for your attention

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